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Time-stepping methods for large scale differential variational inequalities (DVI) in nonsmooth dynamics

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1. Plan

1. Complementarity and variational inequalities.
2. Differential Variational Inequalities (DVI) and nonsmooth dynamics.
3. Time-stepping methods for nonsmooth dynamics.
4. Iterative (~ projected Gauss-Seidel) methods for the subproblem.
5. Numerical Examples.
6. Some GPU calculation examples.

1. Complementarity and Variational Inequalities.

Complementarity-Complementary Variables.

Are variables that satisfy

$$s \geq 0, x \geq 0, s^T x = 0 \leftrightarrow 0 \leq s \perp x \geq 0$$

Their most common occurrence is perhaps in the optimality conditions of problems with bound constraints

$$\min_{x \geq 0} F(x) \Rightarrow \nabla_x F(x) - s = 0, 0 \leq s \perp x \geq 0$$

But their modeling power exceeds optimization since **they can quantify alternatives.**

- Example : Normal force – normal separation

Most common algebraic format: linear complementarity problems, LCP

$$s = \mathcal{M}x + q(F(x)), s \geq 0, x \geq 0, s^T x = 0.$$

- Examples: Linear and Quadratic Programming.
- Important classes of matrices: **PSD** ($x^T \mathcal{M}x \geq 0, \forall x$) and **copositive** ($x^T \mathcal{M}x \geq 0, \forall x \geq 0$).
- **LCP**'s involving copositive matrices do not have a solution in general.
- Let \mathcal{M} be copositive. If, $x \geq 0$ and $x^T \mathcal{M}x = 0$ implies $q^T x \geq 0$, then the **LCP** has a solution that can be found by Lemke's algorithm.

Variational Inequalities and connection to complementarity.

Problem: Let $F : \mathbb{R}^{n+m} \rightarrow \mathbb{R}^m$, $F \in \mathcal{C}^2$, and $\mathcal{K} \subset \mathbb{R}^m$ be a convex set. Find $y \in \mathbb{R}^m$ such that

$$\langle F(x, y), v - y \rangle \geq 0, \quad \forall v \in \mathcal{K}.$$

x are the design variables, y are the state variables. **Solution set of the variational inequality:** $\mathcal{S}(x)$.

$\mathcal{K} = \{v \in \mathbb{R}^m \mid v \geq b\}$, for some vector $b \in \mathbb{R}^m$, the parameterized variational inequality can be represented as

$$\begin{aligned} F(x, y) &\geq 0, \\ y &\geq b, \\ (y - b)^T F(x, y) &= 0. \end{aligned}$$

2. Nonsmooth contact dynamics-Differential Variational Inequalities (DVI)



Nonsmooth contact dynamics—what is it?

- Differential problem with variational inequality constraints –

DVI

Newton Equations

Non-Penetration Constraints

$$M \frac{dv}{dt} = \sum_{j=1,2,\dots,p} \left(c_n^{(j)} n^{(j)} + \beta_1^{(j)} t_1^{(j)} + \beta_2^{(j)} t_2^{(j)} \right) + f_c(q, v) + k(t, q, v)$$

$$\frac{dq}{dt} = \Gamma(q)v \quad \leftarrow \text{Generalized Velocities}$$

$$c_n^{(j)} \geq 0 \perp \Phi^{(j)}(q) \geq 0, \quad j = 1, 2, \dots, p$$

$$\left(\beta_1^{(j)}, \beta_2^{(j)} \right) = \operatorname{argmin}_{\mu^{(j)} c_n^{(j)} \geq \sqrt{(\beta_1^{(j)} + \beta_2^{(j)})^2}} \left[\left(v^T t_1^{(j)} \right) \beta_1 + \left(v^T t_2^{(j)} \right) \beta_2 \right]$$

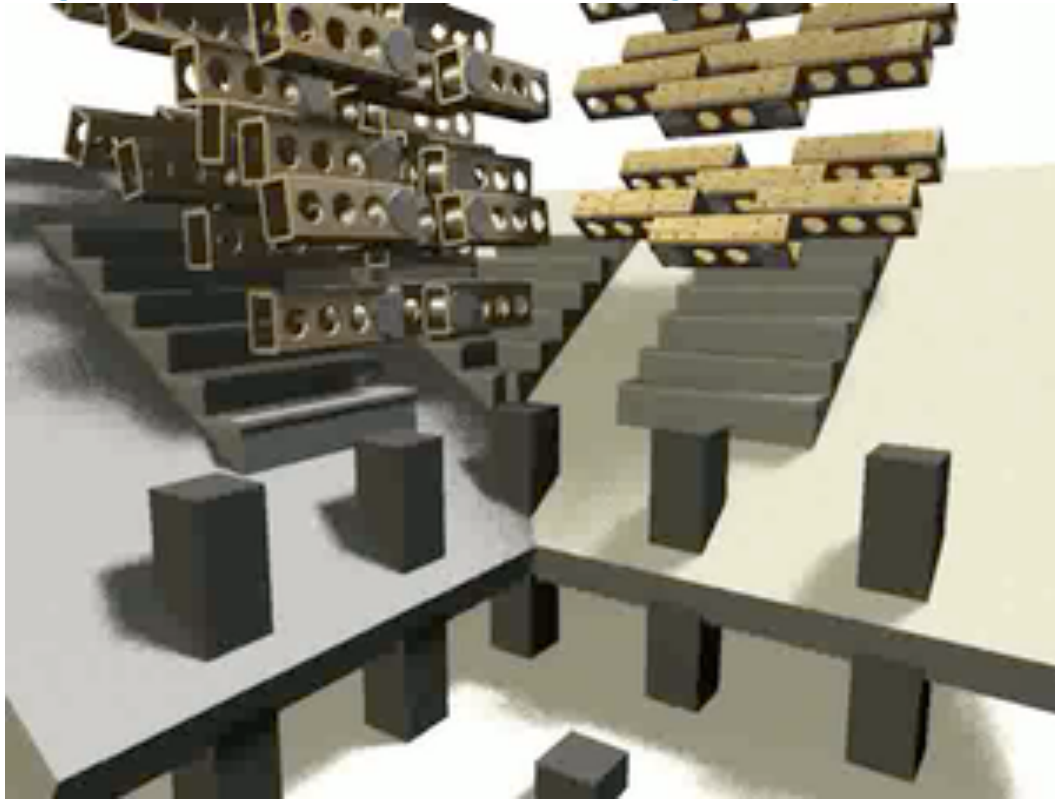
Friction Model

- Truly, a Differential Problem with Equilibrium (parametric VI) Constraints AND complementarity constraints

Differential Variational Inequalities— why do it?

- Contact Dynamics.
 - Rigid-Bodies: Differential Operator is ODE.
 - Deformable Bodies: Differential Operator is PDE.
 - Granular Flow, Masonry Stability, Rock Dynamics...
- Finance: Option Pricing-- American Options. PDE-based.
- Dynamics of multicristalline materials: evolution of the boundary between phases.
- Porous Media Flow.
- See Luo, Pang et al, and Kinderlehrer and Stampacchia Monographs..

Or, just for fun *Physics-based VR*



Note: **real-time** simulation

- Implication:
Speed and
Stability more
weight than of
accuracy.

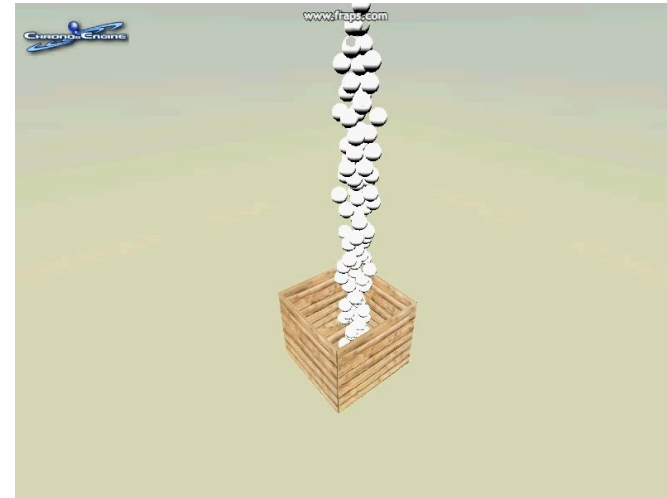
- This “fun” is serious business in the US,
- One of the main drivers of new architectures (GPU, Ageia); huge user community

Question 1: Should we do smoothing?

- Recall, DVI (for $C=R^+$) \longrightarrow
$$\dot{x} = f(t, x(t), u(t));$$
$$u \geq 0 \perp F(t, x(t), u(t)) \geq 0$$
- Smoothing \longrightarrow
$$\dot{x} = f(t, x(t), u(t));$$
$$u_i F_i(t, x(t), u(t)) = \varepsilon, \quad i = 1, 2, \dots, n_u$$
- Followed by forward Euler. \longrightarrow
Easy to implement!!
$$u_i^n F_i(t^{n-1}, x^{n-1}, u^{n-1}) = \varepsilon, \quad i = 1, 2, \dots, n_u$$
$$x^{n+1} = x^n + hf(t^n, x^n, u^n);$$
- Compare with the complexity of time-stepping \longrightarrow
$$x^{n+1} = x^n + hf(t^{n+1}, x^{n+1}, u^{n+1});$$
- But does it give good results?
$$u^{n+1} \geq 0 \perp F(t^{n+1}, x^{n+1}, u^{n+1}) \geq 0$$

Applying ADAMS to granular flow

- ADAMS is the workhorse of engineering dynamics.
- ADAMS/View Procedure for simulating.
- Spheres: diameter of 60 mm and a weight of 0.882 kg.
- Forces: smoothing with stiffness of $1E5$, force exponent of 2.2, damping coefficient of 10.0, and a penetration depth of 0.1



ADAMS versus ChronoEngine

Table 1: Number of rigid bodies v. CPU time in ADAMS

Number of Spheres	Max Number of Mutual Contacts [-]	CPU time (seconds)
1	1	0.41
2	3	3.3
4	14	7.75
8	44	25.36
16	152	102.78
32	560	644.4

The following graph shows the nonlinear increase in the CPU time as the number of colliding bodies increases.

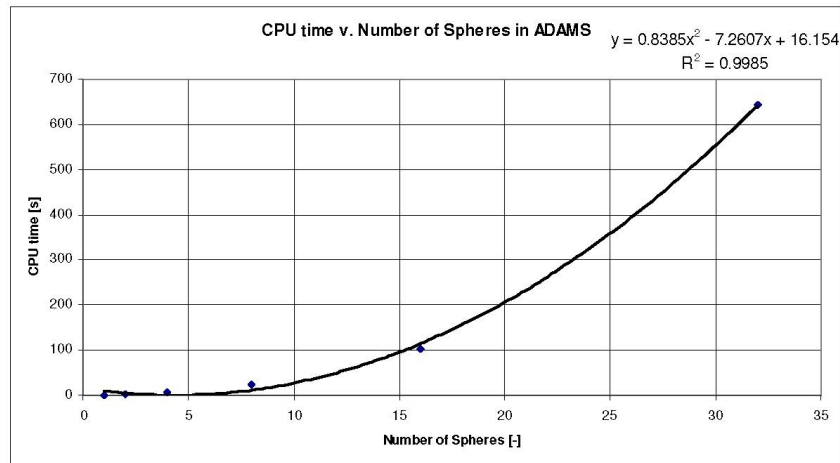
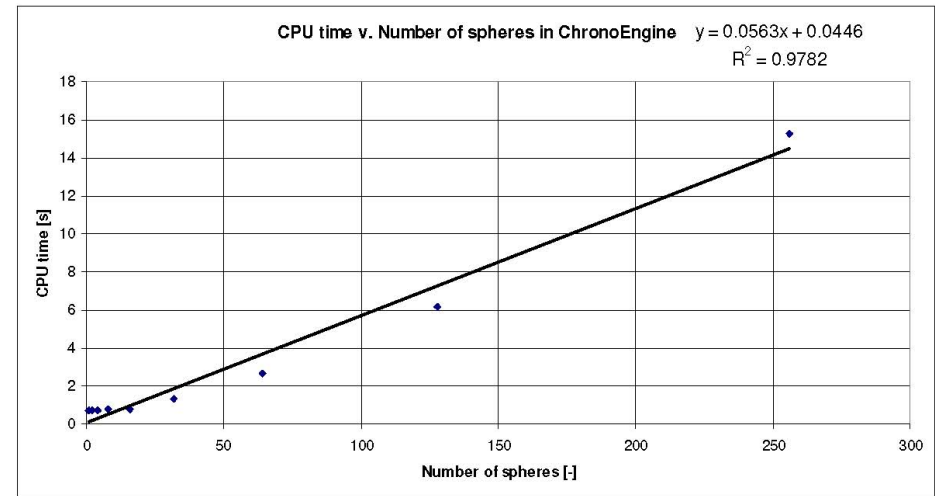


Table 2: Number of rigid bodies v. CPU time in ChronoEngine

Number of Spheres	Max Number of Mutual Contacts [-]	CPU time (seconds)
1	1	0.70
2	3	0.73
4	14	0.73
8	44	0.76
16	152	0.82
32	560	1.32
64	2144	2.65
128	8384	6.17
256	33152	15.30



Conclusion 1: Often, time stepping is more promising,

Recall: Nonsmooth contact dynamics

- Differential problem with equilibrium constraints – DPEC.

$$M \frac{dv}{dt} = \sum_{j=1,2,\dots,p} \left(c_n^{(j)} n^{(j)} + \beta_1^{(j)} t_1^{(j)} + \beta_2^{(j)} t_2^{(j)} \right) + f_c(q, v) + k(t, q, v)$$

$$\frac{dq}{dt} = v$$

$$c_n^{(j)} \geq 0 \quad \perp \quad \Phi^{(j)}(q) \geq 0, \quad j = 1, 2, \dots, p$$

$$\left(\beta_1^{(j)}, \beta_2^{(j)} \right) = \operatorname{argmin}_{\mu^{(j)} c_n^{(j)} \geq \sqrt{(\beta_1^{(j)} + \beta_2^{(j)})^2}} \left[\left(v^T t_1^{(j)} \right) \beta_1 + \left(v^T t_2^{(j)} \right) \beta_2 \right]$$

Friction Model

Options and challenges for methods with no smoothing

- Piecewise DAE (Haug, 86)
 - Plus : Uses well understood DAE technology
 - Minus: The density of switches, switching consistency, and Painleve are problems.
- Acceleration-force time-stepping (Glocker & Pfeiffer, 1992, Pang & Trinkle, 1995)
 - Plus: No consistency problem.
 - Minus: Density of switches and Painleve.
- Velocity-impulse time-stepping. (Moreau, 196*, 198*, 199*, Stewart and Trinkle, 1996, Anitescu & Potra, 1997)
 - Plus: No consistency, or Painleve. Some have fixed time stepping (Moreau, 198*, Anitescu & Hart 04, Anitescu, 06).
 - Minus: Nonzero restitution coefficient is tough—but its value is disputable in **any case**

3. Time-stepping methods

Conic Complementarity IS NATURAL in Coulomb Models.

- Coulomb model.

$$\left(\beta_1^{(j)}, \beta_2^{(j)} \right) = \operatorname{argmin}_{\mu^{(j)} c_n^{(j)} \geq \sqrt{(\beta_1^{(j)} + \beta_2^{(j)})^2}} \left[\left(v^T t_1^{(j)} \right) \beta_1 + \left(v^T t_2^{(j)} \right) \beta_2 \right]$$

$$K = \left\{ (x, y, z) \mid \mu^{(j)} z \geq \sqrt{y^2 + x^2} \right\} \quad K^* = \left\{ (x, y, z) \mid z \geq \mu^{(j)} \sqrt{y^2 + x^2} \right\}$$

$$\begin{pmatrix} c_n^{(j)} \\ \beta_1^{(j)} \\ \beta_2^{(j)} \end{pmatrix} \in K \quad \perp \quad \begin{pmatrix} \mu^{(j)} \sqrt{\left(v^T t_1^{(j)} \right)^2 + \left(v^T t_2^{(j)} \right)^2} \\ v^T t_1^{(j)} \\ v^T t_2^{(j)} \end{pmatrix} \in K^*$$

- Most previous approaches discretize friction cone to use LCP...
- Question 2: Can we still get convergence but not do that?

Time stepping scheme -- original

- A measure differential inclusion solution can be obtained by time-stepping (Stewart, 1998, Anitescu 2006)

$$M(\mathbf{v}^{(l+1)} - \mathbf{v}^l) = \sum_{i \in \mathcal{A}(q^{(l)}, \epsilon)} (\gamma_n^i \mathbf{D}_n^i + \gamma_u^i \mathbf{D}_u^i + \gamma_v^i \mathbf{D}_v^i) + \sum_{i \in \mathcal{G}_B} (\gamma_b^i \nabla \Psi^i) + h \mathbf{f}_t(t^{(l)}, \mathbf{q}^{(l)}, \mathbf{v}^{(l)})$$

Speeds

Reaction impulses

Forces

Stabilization terms

$$0 = \frac{1}{h} \Psi^i(\mathbf{q}^{(l)}) + \nabla \Psi^{iT} \mathbf{v}^{(l+1)} + \frac{\partial \Psi^i}{\partial t}, \quad i \in \mathcal{G}_B$$

Bilateral constraint equations

$$0 \leq \frac{1}{h} \Phi^i(\mathbf{q}^{(l)}) + \nabla \Phi^{iT} \mathbf{v}^{(l+1)}$$

Contact constraint equations

$$\perp \quad \gamma_n^i \geq 0, \quad i \in \mathcal{A}(q^{(l)}, \epsilon)$$

COMPLEMENTARITY!

$$(\gamma_u^i, \gamma_v^i) = \operatorname{argmin}_{\mu^i \gamma_n^i \geq \sqrt{(\gamma_u^i)^2 + (\gamma_v^i)^2}} \quad i \in \mathcal{A}(q^{(l)}, \epsilon)$$

$$[\mathbf{v}^T (\gamma_u \mathbf{D}_u^i + \gamma_v \mathbf{D}_v^i)]$$

Coulomb 3D friction model

$$\mathbf{q}^{(l+1)} = \mathbf{q}^{(l)} + h \mathbf{v}^{(l+1)},$$

Pause: Constraint Stabilization

- Compared to original scheme

$$\nabla\Phi(q^{(l)})^T v^{(l+1)} \geq 0 \implies \Phi^{(j)}(q^{(l)}) + \gamma h_l \nabla\Phi(q^{(l)})^T v^{(l+1)} \geq 0.$$

$$\nabla\Theta(q^{(l)})^T v^{(l+1)} = 0 \implies \Theta^{(j)}(q^{(l)}) + \gamma h_l \nabla\Theta(q^{(l)})^T v^{(l+1)} = 0.$$

- Allows fixed time steps for plastic collisions.
- How do we know it is achieved? Infeasibility is one order better than accuracy ($O(h^2)$)

Time Stepping -- Convex Relaxation

- A modification (relaxation, to get convex QP with conic constraints):

$$M(\mathbf{v}^{(l+1)} - \mathbf{v}^l) = \sum_{i \in \mathcal{A}(q^{(l)}, \epsilon)} (\gamma_n^i \mathbf{D}_n^i + \gamma_u^i \mathbf{D}_u^i + \gamma_v^i \mathbf{D}_v^i) + \sum_{i \in \mathcal{G}_B} (\gamma_b^i \nabla \Psi^i) + h \mathbf{f}_t(t^{(l)}, \mathbf{q}^{(l)}, \mathbf{v}^{(l)})$$

$$0 = \frac{1}{h} \Psi^i(\mathbf{q}^{(l)}) + \nabla \Psi^{iT} \mathbf{v}^{(l+1)} + \frac{\partial \Psi^i}{\partial t}, \quad i \in \mathcal{G}_B$$

$$0 \leq \frac{1}{h} \Phi^i(\mathbf{q}^{(l)}) + \nabla \Phi^{iT} \mathbf{v}^{(l+1)} - \mu^i \sqrt{(\mathbf{D}_u^{i,T} \mathbf{v})^2 + (\mathbf{D}_v^{i,T} \mathbf{v})^2}$$

$$\perp \quad \gamma_n^i \geq 0, \quad i \in \mathcal{A}(q^{(l)}, \epsilon)$$

$$(\gamma_u^i, \gamma_v^i) = \operatorname{argmin}_{\mu^i \gamma_n^i \geq \sqrt{(\gamma_u^i)^2 + (\gamma_v^i)^2}} \quad i \in \mathcal{A}(q^{(l)}, \epsilon)$$

$$[\mathbf{v}^T (\gamma_u \mathbf{D}_u^i + \gamma_v \mathbf{D}_v^i)]$$

$$\mathbf{q}^{(l+1)} = \mathbf{q}^{(l)} + h \mathbf{v}^{(l+1)},$$

(For small μ and/or small speeds, almost no one-step differences from the Coulomb theory)

But In any case, converges to same MDI as unrelaxed scheme.

[see M.Anitescu, "Optimization Based Simulation of Nonsmooth Rigid Body Dynamics"]

Pause: what does convergence mean here?

We must now assign a meaning to

$$M \frac{dv}{dt} - f_c(q, v) - k(t, q, v) \in FC(q).$$

Definition If ν is a measure and $K(\cdot)$ is a convex-set valued mapping, we say that v satisfies the differential inclusions

$$\frac{dv}{dt} \in K(t)$$

if, for all continuous $\phi \geq 0$ with compact support, not identically 0, we have that

$$\frac{\int \phi(t) \nu(dt)}{\int \phi(t) dt} \in \bigcup_{\tau: \phi(\tau) \neq 0} K(\tau).$$

Pause(2) : What does convergence mean here?

H1 The functions $n^{(j)}(q), t_1^{(j)}(q), t_2^{(j)}(q)$ are smooth and globally Lipschitz, and they are bounded in the 2-norm.

H2 The mass matrix M is positive definite.

H3 The external force increases at most linearly with the velocity and position.

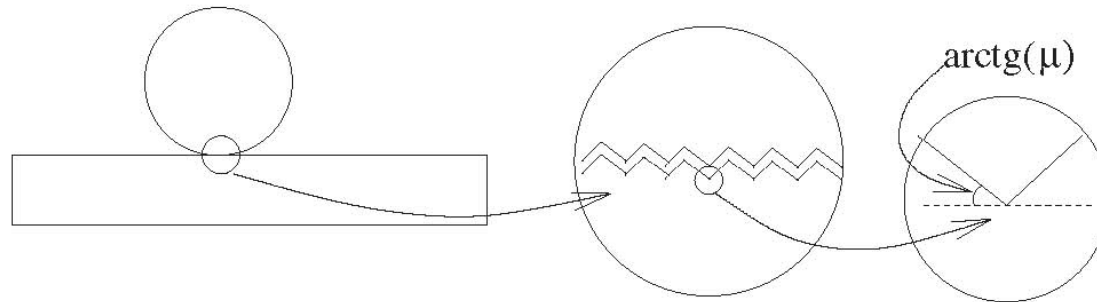
H4 The uniform pointed friction cone assumption holds.

Then there exists a subsequence $h_k \rightarrow 0$ where

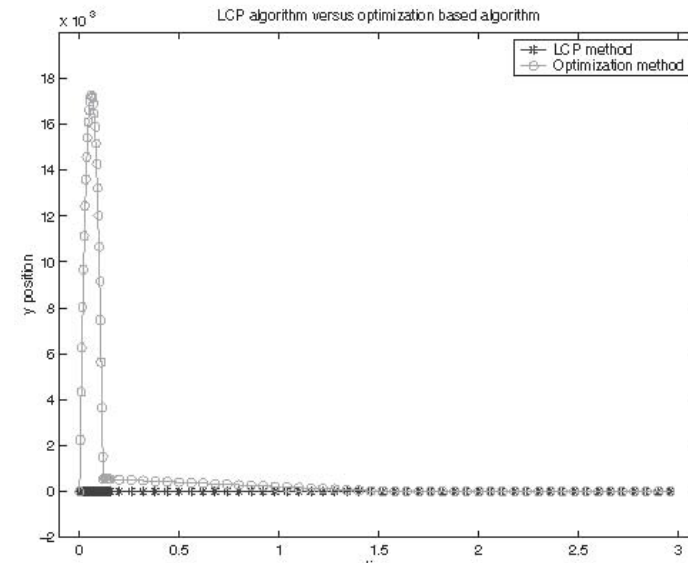
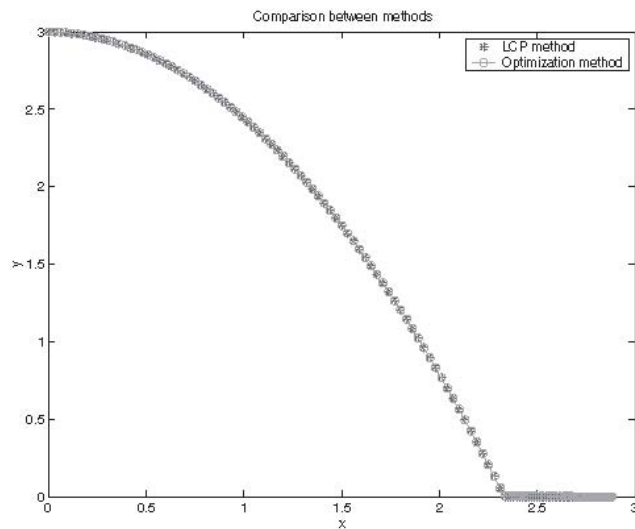
- $q^{h_k}(\cdot) \rightarrow q(\cdot)$ uniformly.
- $v^{h_k}(\cdot) \rightarrow v(\cdot)$ pointwise a.e.
- $dv^{h_k}(\cdot) \rightarrow dv(\cdot)$ weak * as Borel measures. in $[0, T]$, and every such subsequence converges to a solution $(q(\cdot), v(\cdot))$ of **MDI**.

What is physical meaning of the relaxation?

■ Origin



■ Behavior



Further insight.

- The key is the combination between relaxation and constraint stabilization.

$$0 \leq \frac{1}{h} \Phi^{(j)}(q^{(l)}) + \nabla_q \Phi^{(j)}(q^{(l)}) v^{(l+1)} - \mu^{(j)} \sqrt{\left(D_u^{l,t} v\right)^2 + \left(D_v^{l,t} v\right)^2}$$

- If the time step is smaller than the variation in velocity then the gap function settles at

$$0 \approx \frac{1}{h} \Phi^{(j)}(q^{(l)}) - \mu^{(j)} \sqrt{\left(D_u^{l,t} v\right)^2 + \left(D_v^{l,t} v\right)^2}$$

- So the solution is the same as the original scheme for a slightly perturbed gap function.....

Cone complementarity

- Aiming at a more compact formulation:

$$\mathbf{b}_A = \left\{ \frac{1}{h} \Phi^{i_1}, 0, 0, \frac{1}{h} \Phi^{i_2}, 0, 0, \dots, \frac{1}{h} \Phi^{i_{n_A}}, 0, 0 \right\}$$

$$\gamma_A = \left\{ \gamma_n^{i_1}, \gamma_u^{i_1}, \gamma_v^{i_1}, \gamma_n^{i_2}, \gamma_u^{i_2}, \gamma_v^{i_2}, \dots, \gamma_n^{i_{n_A}}, \gamma_u^{i_{n_A}}, \gamma_v^{i_{n_A}} \right\}$$

$$\mathbf{b}_B = \left\{ \frac{1}{h} \Psi^1 + \frac{\partial \Psi^1}{\partial t}, \frac{1}{h} \Psi^2 + \frac{\partial \Psi^2}{\partial t}, \dots, \frac{1}{h} \Psi^{n_B} + \frac{\partial \Psi^{n_B}}{\partial t} \right\}$$

$$\gamma_B = \left\{ \gamma_b^1, \gamma_b^2, \dots, \gamma_b^{n_B} \right\}$$

$$D_A = [D^{i_1} | D^{i_2} | \dots | D^{i_{n_A}}], \quad i \in \mathcal{A}(\mathbf{q}^l, \epsilon) \quad D^i = [D_n^i | D_u^i | D_v^i]$$

- $D_B = [\nabla \Psi^{i_1} | \nabla \Psi^{i_2} | \dots | \nabla \Psi^{i_{n_B}}], \quad i \in \mathcal{G}_B$

$$\mathbf{b}_E \in \mathbb{R}^{n_E} = \{\mathbf{b}_A, \mathbf{b}_B\}$$

$$\gamma_E \in \mathbb{R}^{n_E} = \{\gamma_A, \gamma_B\}$$

$$D_E = [D_A | D_B]$$

Cone complementarity

- Also define:

$$\tilde{\mathbf{k}}^{(l)} = M\mathbf{v}^{(l)} + h\mathbf{f}_t(t^{(l)}, \mathbf{q}^{(l)}, \mathbf{v}^{(l)})$$

$$N = D_{\mathcal{E}}^T M^{-1} D_{\mathcal{E}}$$

$$\mathbf{r} = D_{\mathcal{E}}^T M^{-1} \tilde{\mathbf{k}} + \mathbf{b}_{\mathcal{E}}$$

- Then:

$$\begin{aligned}
 M(\mathbf{v}^{(l+1)} - \mathbf{v}^l) &= \sum_{i \in \mathcal{A}(q^{(l)}, \epsilon)} (\gamma_n^i D_n^i + \gamma_u^i D_u^i + \gamma_v^i D_v^i) + \\
 &\quad + \sum_{i \in \mathcal{G}_B} (\gamma_b^i \nabla \Psi^i) + h\mathbf{f}_t(t^{(l)}, \mathbf{q}^{(l)}, \mathbf{v}^{(l)}) \\
 0 &= \frac{1}{h} \Psi^i(q^{(l)}) + \nabla \Psi^{iT} \mathbf{v}^{(l+1)} + \frac{\partial \Psi^i}{\partial t}, \quad i \in \mathcal{G}_B \\
 0 &\leq \frac{1}{h} \Phi^i(q^{(l)}) + \nabla \Phi^{iT} \mathbf{v}^{(l+1)} \\
 &\quad \perp \gamma_n^i \geq 0, \quad i \in \mathcal{A}(q^{(l)}, \epsilon) \\
 (\gamma_u^i, \gamma_v^i) &= \operatorname{argmin}_{\mu^i \gamma_n^i \geq \sqrt{(\gamma_u^i)^2 + (\gamma_v^i)^2}} \quad i \in \mathcal{A}(q^{(l)}, \epsilon) \\
 &\quad [\mathbf{v}^T (\gamma_u D_u^i + \gamma_v D_v^i)]
 \end{aligned}$$

This is a CCP,
CONE COMPLEMENTARITY
PROBLEM

becomes..

$$(N\gamma_{\mathcal{E}} + \mathbf{r}) \in -\Upsilon^{\circ} \quad \perp \quad \gamma_{\mathcal{E}} \in \Upsilon$$

Cone complementarity—Decomposable cones.

- Here we introduced the convex cone

$$\Upsilon = \left(\bigoplus_{i \in \mathcal{A}(\mathbf{q}^l, \epsilon)} \mathcal{FC}^i \right) \oplus \left(\bigoplus_{i \in \mathcal{G}_B} \mathcal{BC}^i \right)$$

\mathcal{FC}^i In \mathbb{R}^3 is i -th friction cone
 \mathcal{BC}^i is \mathbb{R}

- ..and its polar cone:

$$\Upsilon^\circ = \left(\bigoplus_{i \in \mathcal{A}(\mathbf{q}^l, \epsilon)} \mathcal{FC}^{i^\circ} \right) \oplus \left(\bigoplus_{i \in \mathcal{G}_B} \mathcal{BC}^{i^\circ} \right)$$

CCP: $(N\gamma_\epsilon + \mathbf{r}) \in -\Upsilon^\circ \perp \gamma_\epsilon \in \Upsilon$

4. Iterative methods for solving conic complementarity problems.

General: The iterative method

- Question 3: How to efficiently solve the Cone Complementarity Problem for large-scale systems?

$$(N\gamma_{\mathcal{E}} + \mathbf{r}) \in -\Upsilon^{\circ} \quad \perp \quad \gamma_{\mathcal{E}} \in \Upsilon$$

- Our method: use a **fixed-point iteration**

$$\gamma^{r+1} = \lambda \Pi_{\Upsilon} (\gamma^r - \omega B^r (N\gamma^r + \mathbf{r} + K^r (\gamma^{r+1} - \gamma^r))) + (1 - \lambda) \gamma^r$$

- with matrices:
- ..and a non-extensive orthogonal projection operator onto feasible set

$$B^r = \begin{bmatrix} \eta_1 I_{n_1} & 0 & \cdots & 0 \\ 0 & \eta_2 I_{n_2} & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \cdots & \eta_{n_k} I_{n_{n_k}} \end{bmatrix}$$

$$N^T = \begin{bmatrix} 0 & K_{12} & K_{13} & \cdots & K_{1n_k} \\ 0 & 0 & K_{23} & \cdots & K_{2n_k} \\ 0 & 0 & 0 & \cdots & K_{3n_k} \\ \vdots & \vdots & \cdots & \ddots & \vdots \\ 0 & 0 & 0 & \cdots & 0 \end{bmatrix}$$

$$\Pi_{\Upsilon} : \mathbb{R}^{n_{\mathcal{E}}} \rightarrow \mathbb{R}^{n_{\mathcal{E}}}$$

General: The iterative method

■ ASSUMPTIONS

- A1 The matrix N of the problem (CCP) is symmetric and positive semi-definite.
- A2 There exists a positive number, $\alpha > 0$ such that, at any iteration r , $r = 0, 1, 2, \dots$, we have that $B^r \succ \alpha I$
- A3 There exists a positive number, $\beta > 0$ such that, at any iteration r , $r = 0, 1, 2, \dots$, we have that $(x^{r+1} - x^r)^T \left((\lambda \omega B^r)^{-1} + K^r - \frac{N}{2} \right) (x^{r+1} - x^r) \geq \beta \|x^{r+1} - x^r\|^2$.

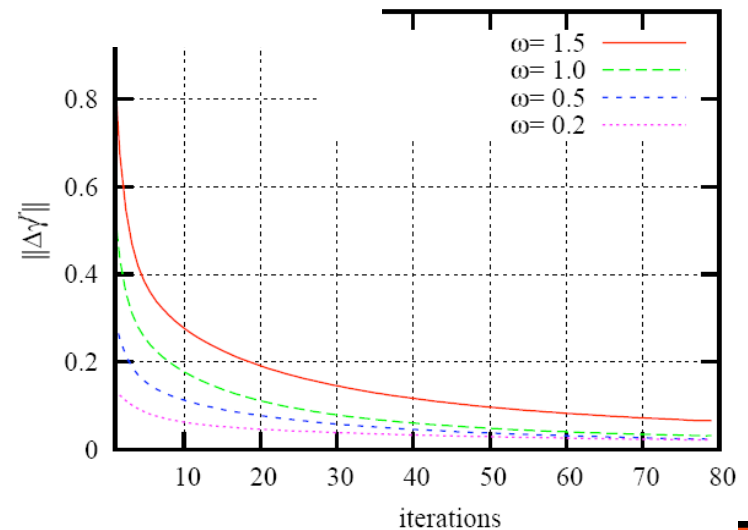
Always satisfied in multibody systems

Essentially free choice, we use identity blocks

Use ω overrelaxation factor to adjust this

■ Under the above assumptions, we can prove **THEOREMS about convergence**.

■ The method produces a **bounded sequence with an unique accumulation point**.



General: Theory

$$(OC) \quad \begin{array}{ll} \min & f(x) = \frac{1}{2}x^T N x + r^T x \\ \text{s.t.} & x_i \in \Upsilon^i, \end{array} \quad i = 1, 2, \dots, n_k.$$

Theorem Assume that $x^0 \in \Upsilon$ and that the sequences of matrices B^r and K^r are bounded. Then we have that

$$f(x^{r+1}) - f(x^r) \leq -\beta \|x^{r+1} - x^r\|^2$$

for any iteration index r , and any accumulation point of the sequence x^r is a solution of (CCP).

Corollary Assume that the friction cone of the configuration is pointed. The algorithm produces a bounded sequence, and any **accumulation point results in the same velocity solution**

- Answer 2: Simple, but first result of this nature for conic constraints—and HIGHLY EFFICIENT

The projection operator is easy and separable

- For each frictional contact constraint:

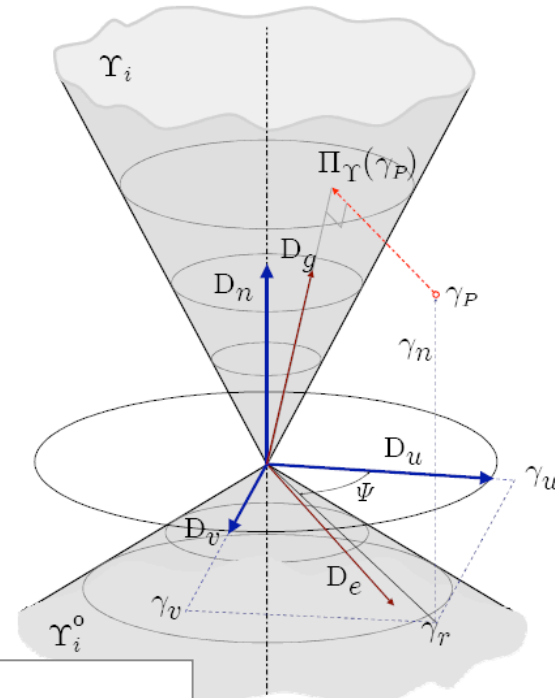
$$\Pi_{\Upsilon} = \left\{ \Pi_{\Upsilon_1}(\gamma_1)^T, \dots, \Pi_{\Upsilon_{n_A}}(\gamma^{n_A})^T, \Pi_b^1(\gamma_b^1), \dots, \Pi_b^{n_B}(\gamma_b^{n_B}) \right\}^T$$

- For each bilateral constraint, simply do nothing.

- The complete operator:

$$\forall i \in \mathcal{A}(\mathbf{q}^{(l)}, \epsilon)$$

$\gamma_r < \mu_i \gamma_n$	$\Pi_i = \gamma_i$
$\gamma_r < -\frac{1}{\mu_i} \gamma_n$	$\Pi_i = \{0, 0, 0\}$
$\gamma_r > \mu_i \gamma_n \wedge \gamma_r > -\frac{1}{\mu_i} \gamma_n$	$\Pi_{i,n} = \frac{\gamma_r \mu_i + \gamma_n}{\mu_i^2 + 1}$
	$\Pi_{i,u} = \gamma_u \frac{\mu_i \Pi_{i,n}}{\gamma_r}$
	$\Pi_{i,v} = \gamma_v \frac{\mu_i \Pi_{i,n}}{\gamma_r}$

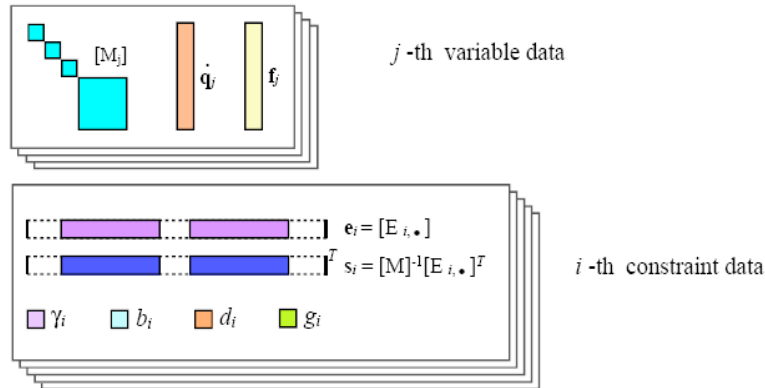


5. Numerical considerations



The algorithm

- Development of an **efficient algorithm** for fixed point iteration:



- *avoid temporary data, exploit **sparsity**. Never compute explicitly the N matrix!*
- *implemented in **incremental** form. Compute only deltas of multipliers.*
- *$O(n)$ **space** requirements and *supports premature termination**
- *for real-time purposes: $O(n)$ **time***

The algorithm is specialized, for minimum memory use!



```

(1) // Pre-compute some data for friction constraints
(2) for i := 1 to nA
(3)   sai = M-1Di
(4)   gai = Di,Tsai
(5)   ηai =  $\frac{3}{\text{Trace}(g_a^i)}$ 
(6) // Pre-compute some data for bilateral constraints
(7) for i := 1 to nB
(8)   sbi = M-1∇Ψi
(9)   gbi = ∇Ψi,Tsbi
(10)  ηbi =  $\frac{1}{g_b^i}$ 
(11)
(12) // Initialize impulses
(13) if warm start with initial guess γε*
(14)   γε0 = γε*
(15) else
(16)   γε0 = 0
(17)
(18) // Initialize speeds
(19) v =  $\sum_{i=1}^{n_A} s_a^i \gamma_a^{i,0} + \sum_{i=1}^{n_B} s_b^i \gamma_b^{i,0} + M^{-1}\tilde{k}$ 

```

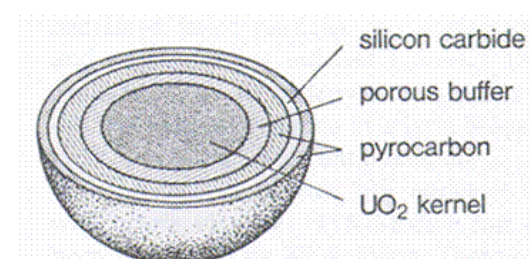
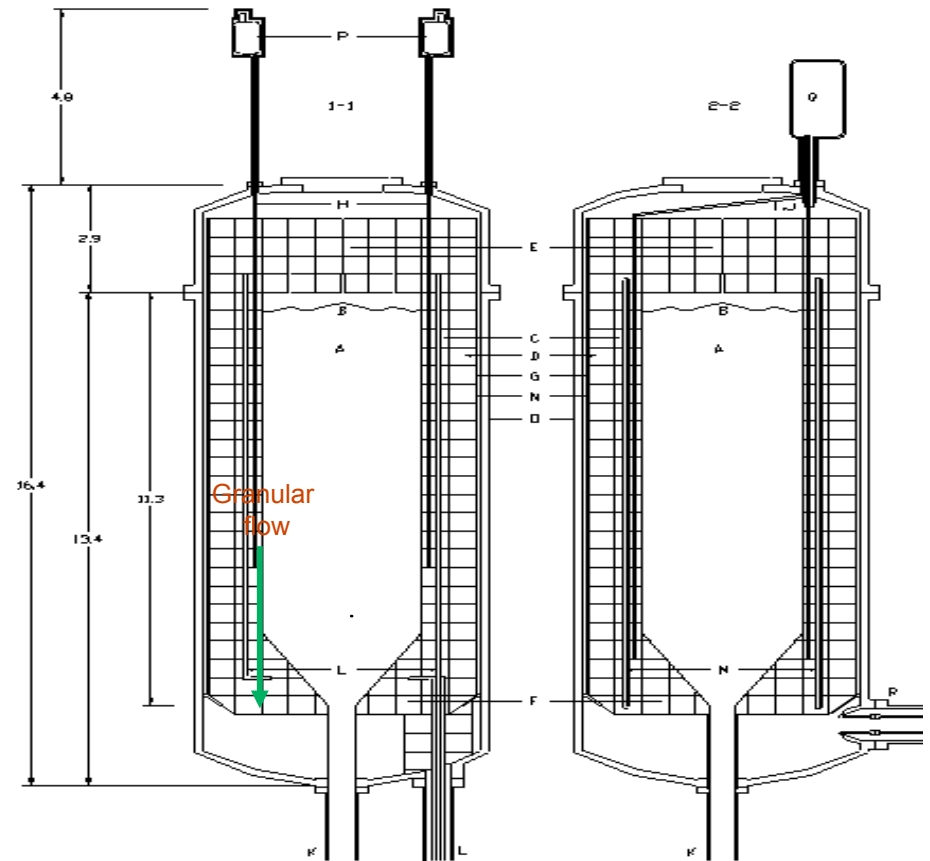
```

(21) // Main iteration loop
(22) for r := 0 to rmax
(23)   // Loop on frictional constraints
(24)   for i := 1 to nA
(25)     δai,r = (γai,r - ωηai(Di,Tvr + bai));
(26)     γai,r+1 = λΠΥ(δai,r) + (1 - λ)γai,r;
(27)     Δγai,r+1 = γai,r+1 - γai,r;
(28)     v := v + sai,TΔγai,r+1.
(29)   // Loop on bilateral constraints
(30)   for i := 1 to nB
(31)     δbi,r = (γbi,r - ωηbi(∇Ψi,Tvr + bbi));
(32)     γbi,r+1 = λΠΥ(δbi,r) + (1 - λ)γbi,r;
(33)     Δγbi,r+1 = γbi,r+1 - γbi,r;
(34)     v := v + sbi,TΔγbi,r+1.
(35)
(36) return γε, v

```

Simulating the PBR nuclear reactor

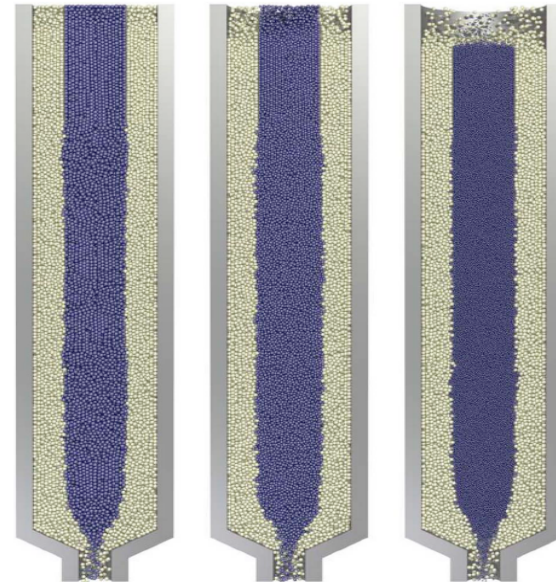
- The **PBR** nuclear reactor:
 - Fourth generation design
 - Inherently safe, by Doppler broadening of fission cross section
 - Helium cooled $> 1000\text{ }^{\circ}\text{C}$
 - Can crack water (mass production of hydrogen)
 - Continuous cycling of **360'000** graphite spheres in a pebble bed



Simulating the PBR nuclear reactor

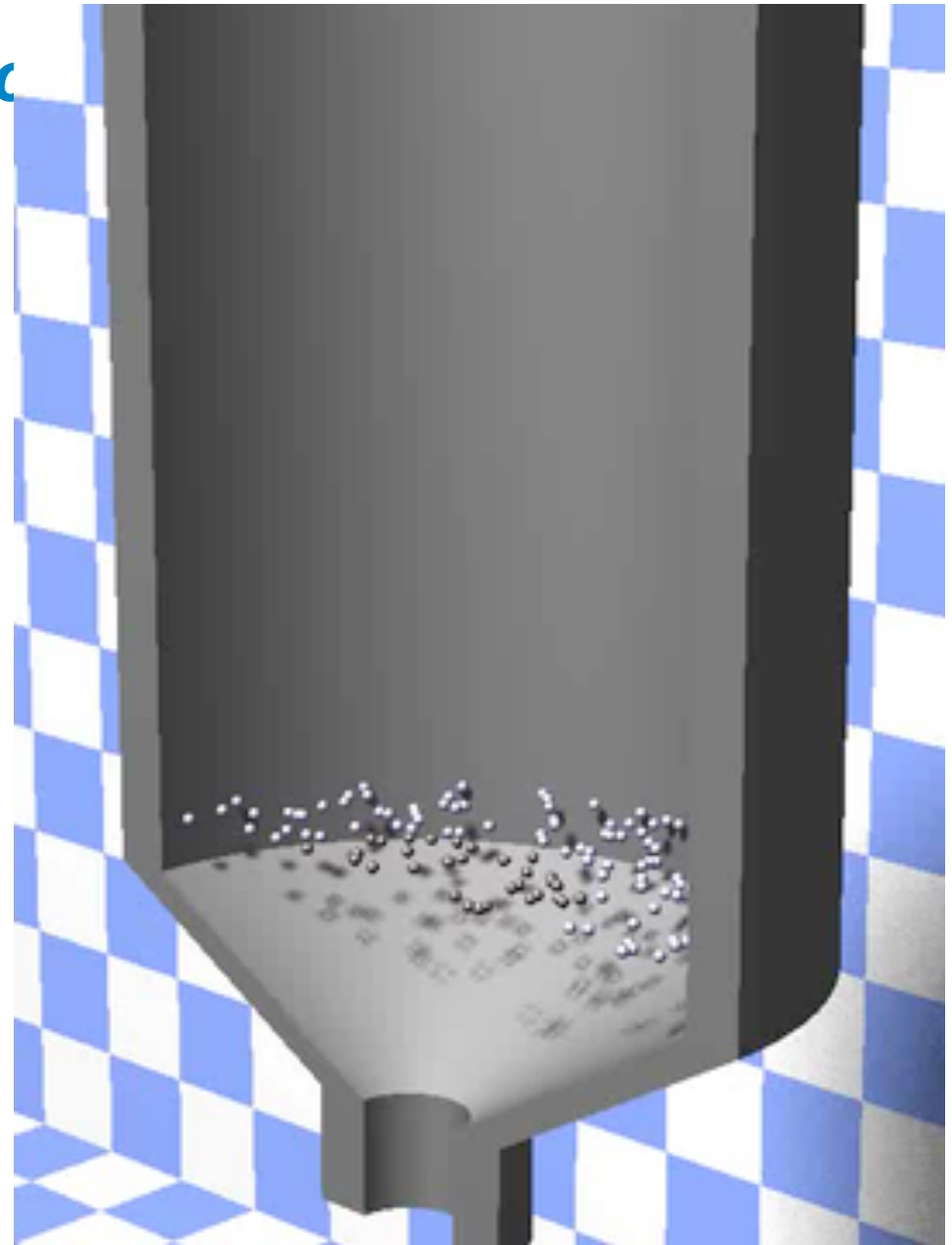
- Problem of **bidisperse granular flow** with **dense packing**.
- Previous attempts: DEM methods on supercomputers at Sandia Labs regularization)
- 40 seconds of simulation for 440,000 pebbles needs 1 week on 64 processors dedicated cluster (Rycroft et al.)

model a frictionless wall, $\mu_w=0.0$. For the current simulations we set $k_t=\frac{2}{7}k_n$ and choose $k_n=2 \times 10^5 \text{ gm/d}$. While this is significantly less than would be realistic for graphite pebbles, where we expect $k_n > 10^{10} \text{ gm/d}$, such a spring constant would be prohibitively computationally expensive, as the time step scales as $\delta t \propto k_n^{-1/2}$ for collisions to be modeled effectively. Previous simulations have shown that

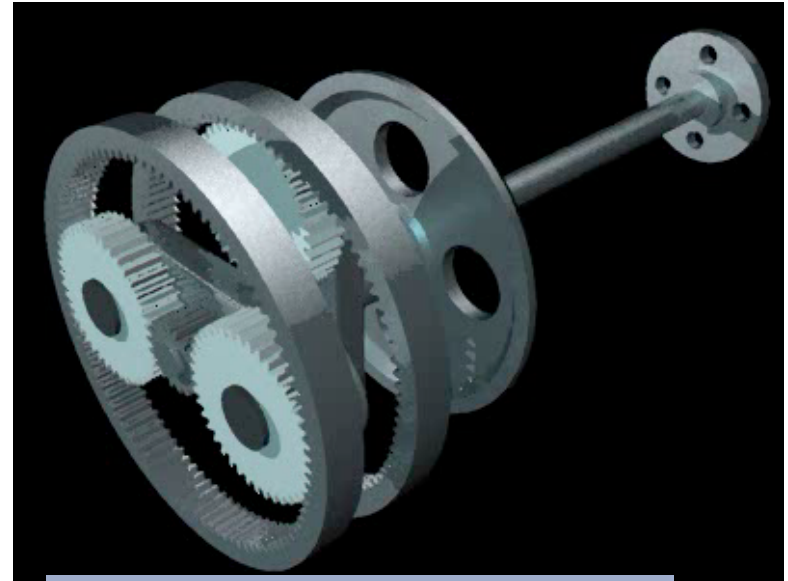
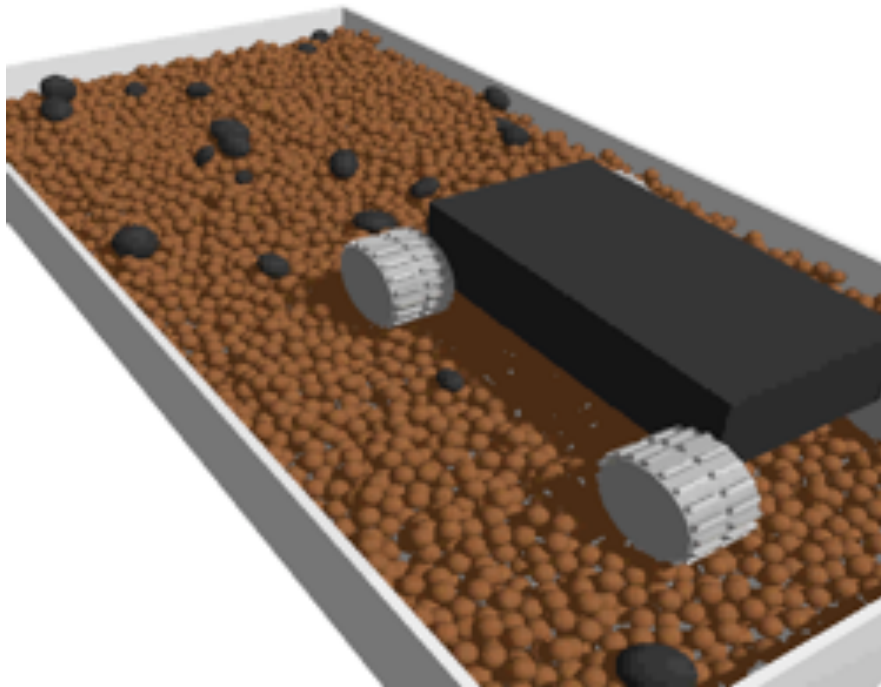


Simulating the PBR nuc

- 160'000 Uranium-Graphite spheres, 600'000 contacts on average
- Two millions of primal variables, six millions of dual variables
- *1 day on a Windows station...*
- But we are limited by the 2GB user mode limit, 64 bit port in progress—but linear scaling..
- We estimate 3CPU days, compare with 450 CPU days for an incomplete solution in 2006 !!!
- Answer 3: Our approach is efficient for large scale!!

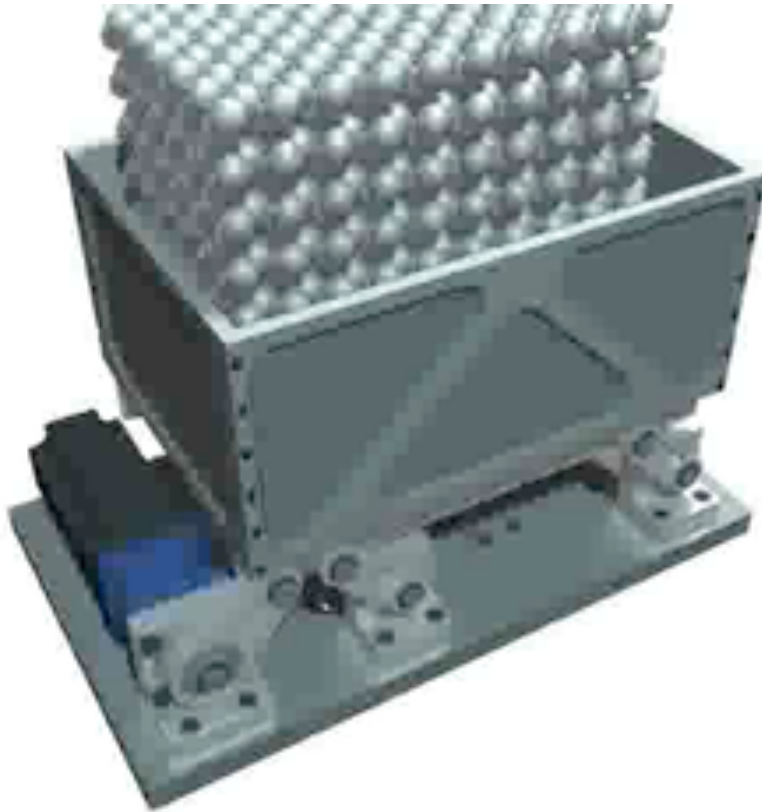


In addition, we can approach efficiently approach many engineering problems (see website for papers)



Examples

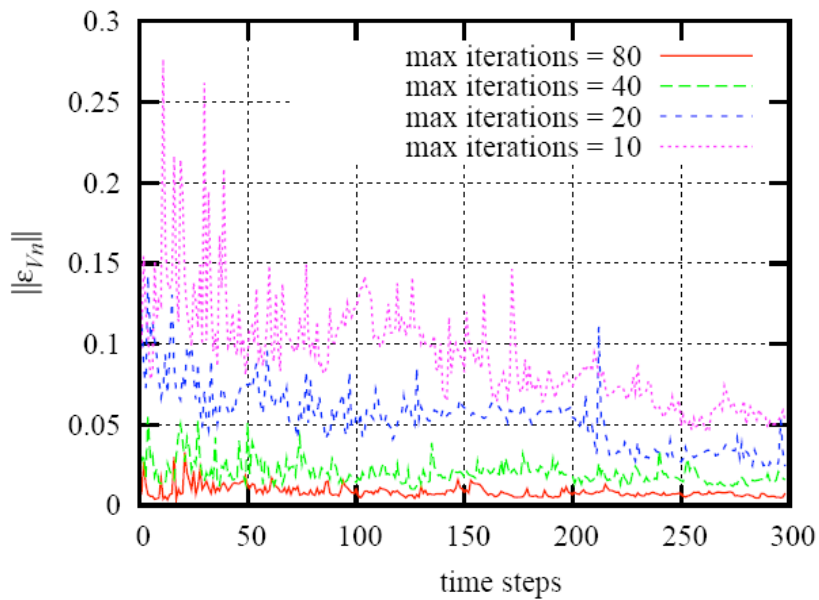
- Example: size-segregation in shaker, with thousands of steel spheres



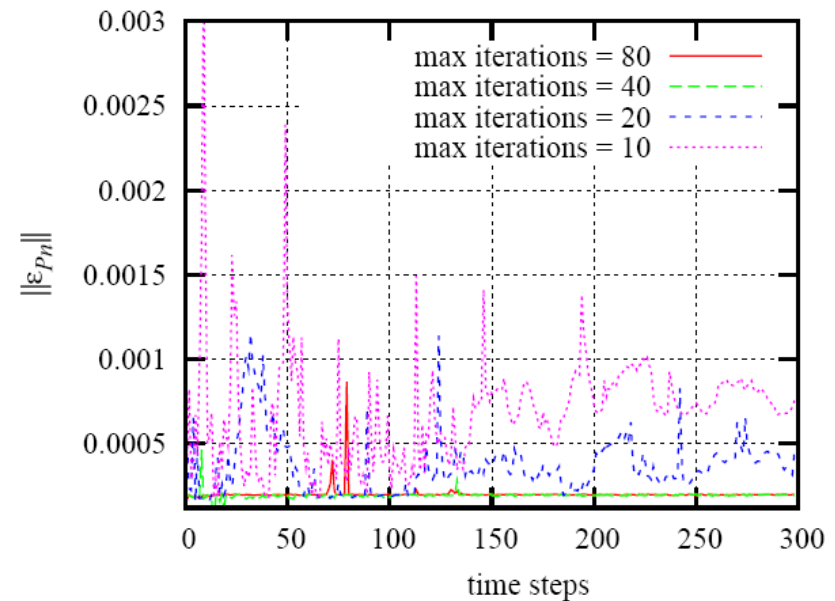
Note: solution beyond reach of Lemke-type LCP solvers!

Tests

■ Feasibility accuracy increases with number of iterations:



Speed violation in constraints

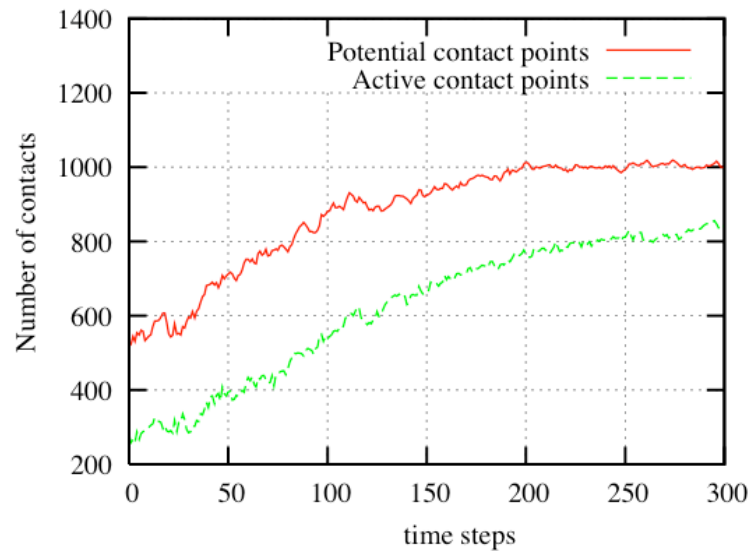


Position error in constraints (penetration)

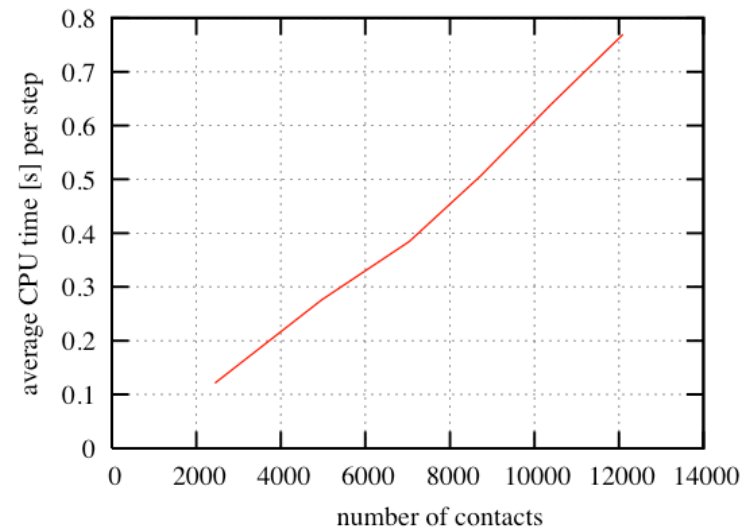
(with example of 300 spheres in shaker)

Tests: Scalability

- CPU effort per contact, since our contacts are the problem variables.
- Penetration error was uniformly no larger than 0.2% of diameter.



Number of contacts in time, 300 spheres

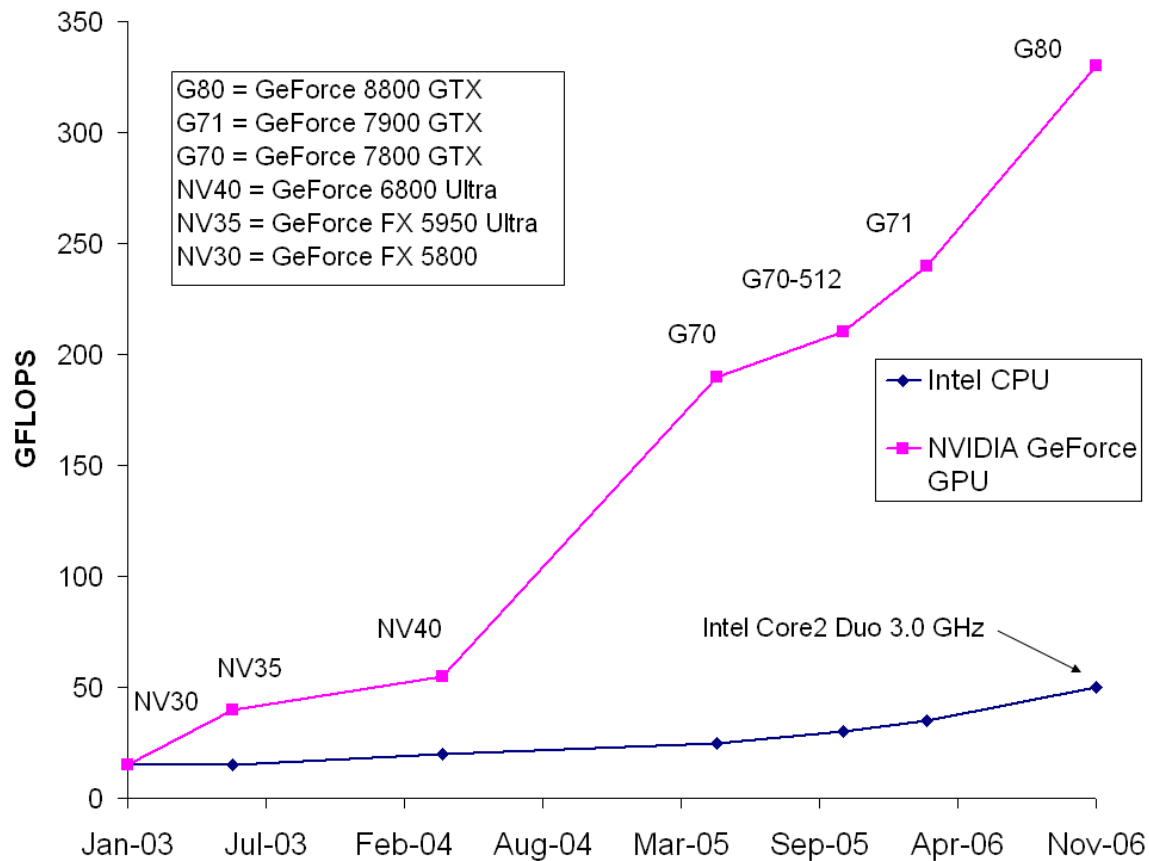


CPU time per step for 300-1500 spheres

6. Initial experiments on graphical processing unit (GPU).

New large scale computational opportunity Graphical Processing Unit

Floating Point Operations per Second for the CPU and GPU



IBM BlueGene/L—GPU comparison

- Entry model: 1024 dual core nodes
- 5.7 Tflop (compare to 0.5 Tflop for NVIDIA Tesla GPU)
- Dedicated OS
- Dedicated power management solution
- Require dedicated IT support
- Price (2007): \$1.4 million
- Same GPU power (2008): 7K!!!

Brick Wall Example...

- Times reported are in seconds for one second long simulation
- GPU: NVIDIA GeForce 8800 GTX



Bricks	Sequential Version	GPU Co-processing Version
1000	43	6
2000	87	10
8000	319	42

Future work

- N non symmetric, but positive semidefinite.
- Parallelizing the algorithms: block Jacobi with Gauss Seidel blocks.
- Asynchronous version of the algorithm, particularly for use with GPU.
- Including a good collision model– here we are at a loss with rigid body theory – may need some measure of deformability.
- Compare with experimental data.

Conclusions

- We have defined a new algorithm for complementarity problems with conic constraints.
- We have shown that it can solve very large problems in granular flow far faster than DEM.
- It is the first iterative algorithm that provably converges for nonsmooth rigid body dynamics.
- Its scalability is decent.
- We have created a multithreaded implementation and GPU port increases computational speed by a factor of 7-8.

References (preprints are at authors' web site)

- M Anitescu, A. Tasora. "An iterative approach for cone complementarity problems for nonsmooth dynamics". Preprint ANL/MCS-P1413-0507, May 2007. Computational Optimization and Applications, to appear.
- M. Anitescu. Optimization-based simulation of nonsmooth dynamics. Mathematical Programming, series A, 105, pp 113–143, 2006.
- Madsen, J., Pechdimaljian, N., and Negrut, D., 2007. Penalty versus complementarity-based frictional contact of rigid bodies: A CPU time comparison. Preprint. TR-2007-05, Simulation-Based Engineering Lab, University of Wisconsin, Madison.